

# Low Profile Tunable Dipole Antennas Using BST Varactors for Biomedical Applications

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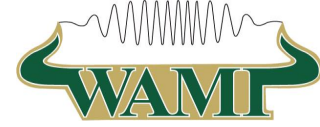
# Outline

- Motivation
- Background
- Previous Related Work
- 1-D Varactor based Tunable Antenna
- Summary
- Acknowledgement
- References

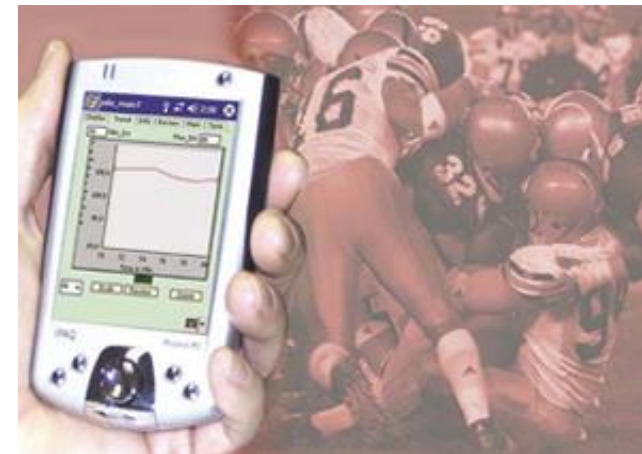
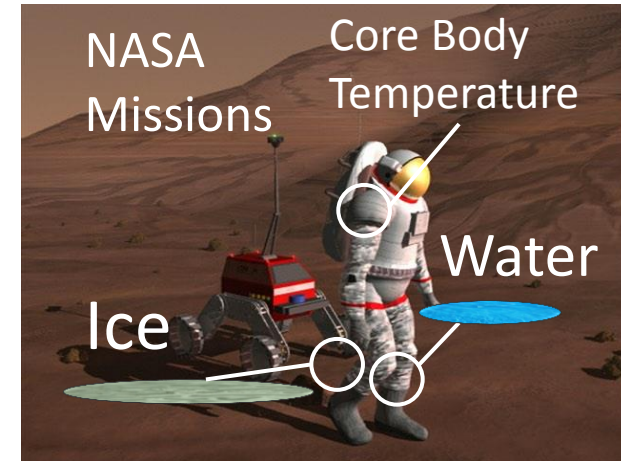
# Low Profile Tunable Dipole Antennas Using BST Varactors for Biomedical Applications

## **MOTIVATION**

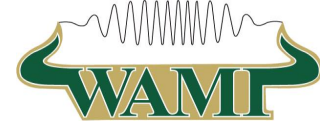
# Motivation



- Design a low profile, conformal, tunable antenna for biomedical applications
- Portable radiometer applications:
  - Health monitoring sensor – astronauts, sports medicine, etc.
  - Remote Underground Thermal Detection

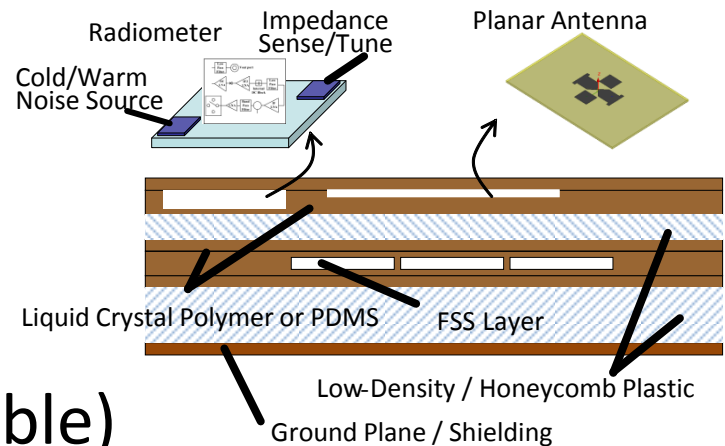
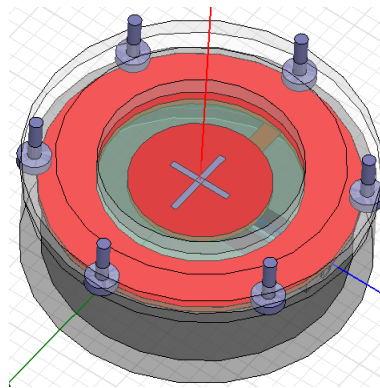


# Motivation(Cont.)



- Antenna Requirements for wearable radiometer:
  - Minimize back-side radiation
  - Large bandwidth ( $\sim 100$  MHz)
  - Low profile and conformal (flexible)
  - Low weight, low cost & low complexity

27 mm height  
 $\sim \lambda/8$  at 1.4 GHz



Cavity-Backed Slot  
Antenna (CBSA)\*  
**Cons: Bulky, heavy.**

[\*] Q. Bonds, T. Weller, B. Roeder and P. Herzig, "A tunable Cavity Backed Slot Antenna (CBSA) for close proximity biomedical sensing applications," in IEEE Microwaves, Communications, Antennas and Electronics Systems, 2009

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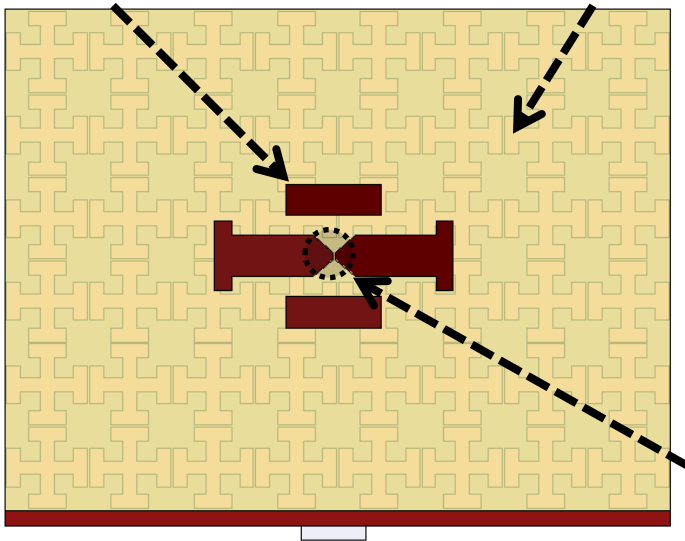
**PREVIOUS WORKS**

# Antenna Structure

Top View

Dipole

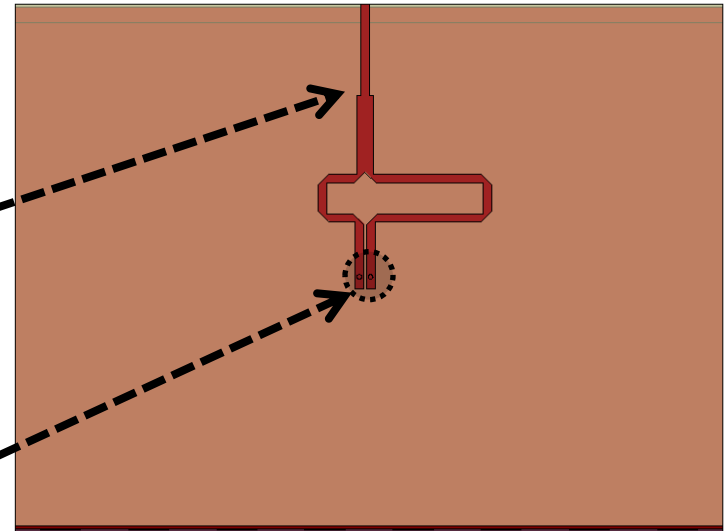
High Impedance Surface



Bottom View

Balun

Live vias



Side View



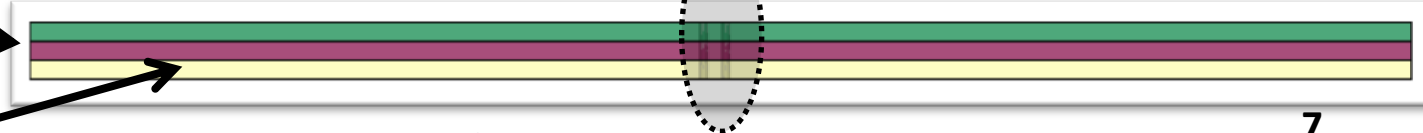
Dipole-Layer 1



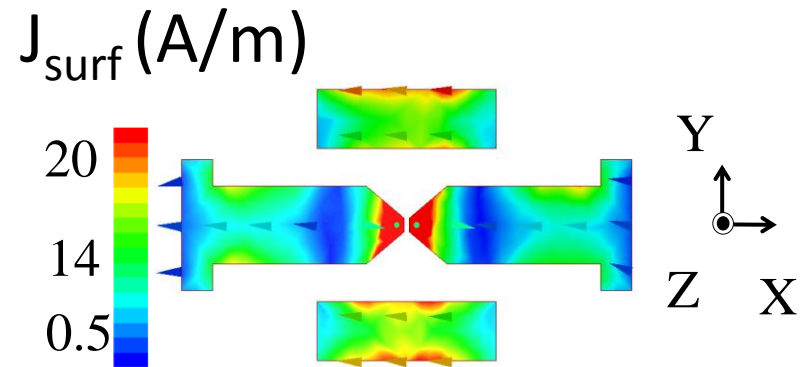
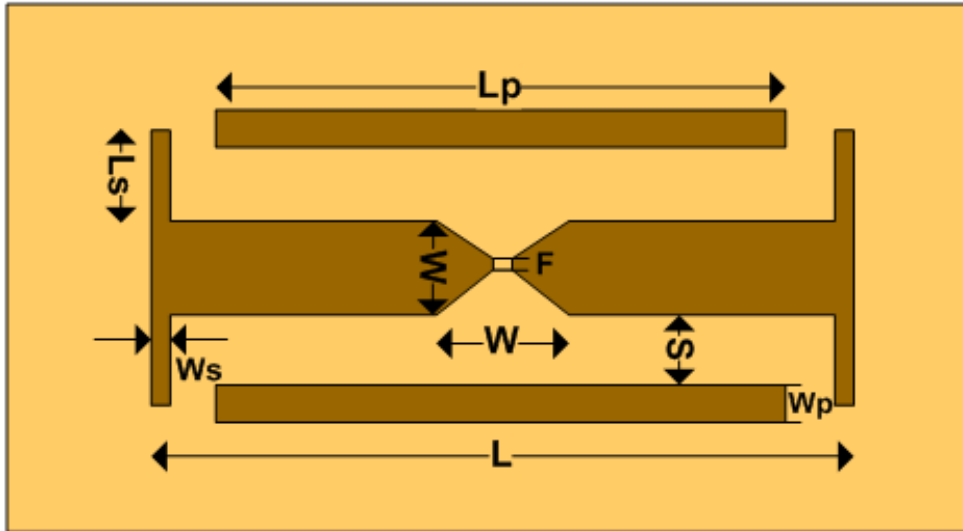
HIS -layer 2



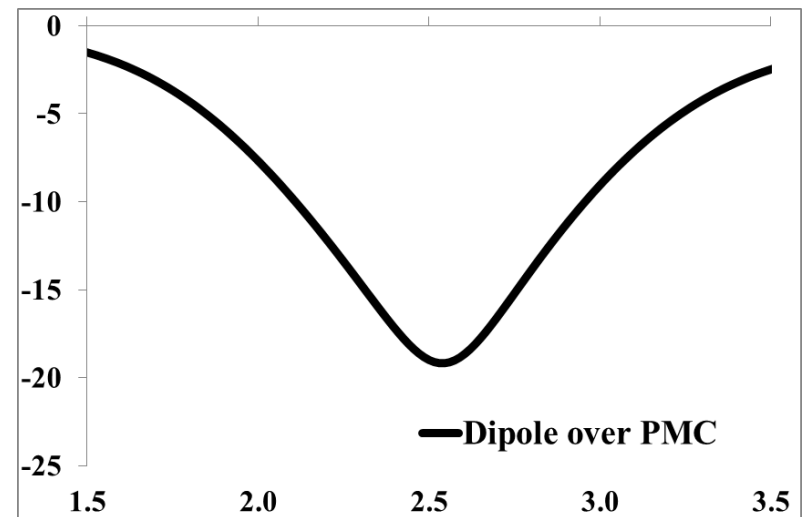
Balun - Layer 3



# Dipole



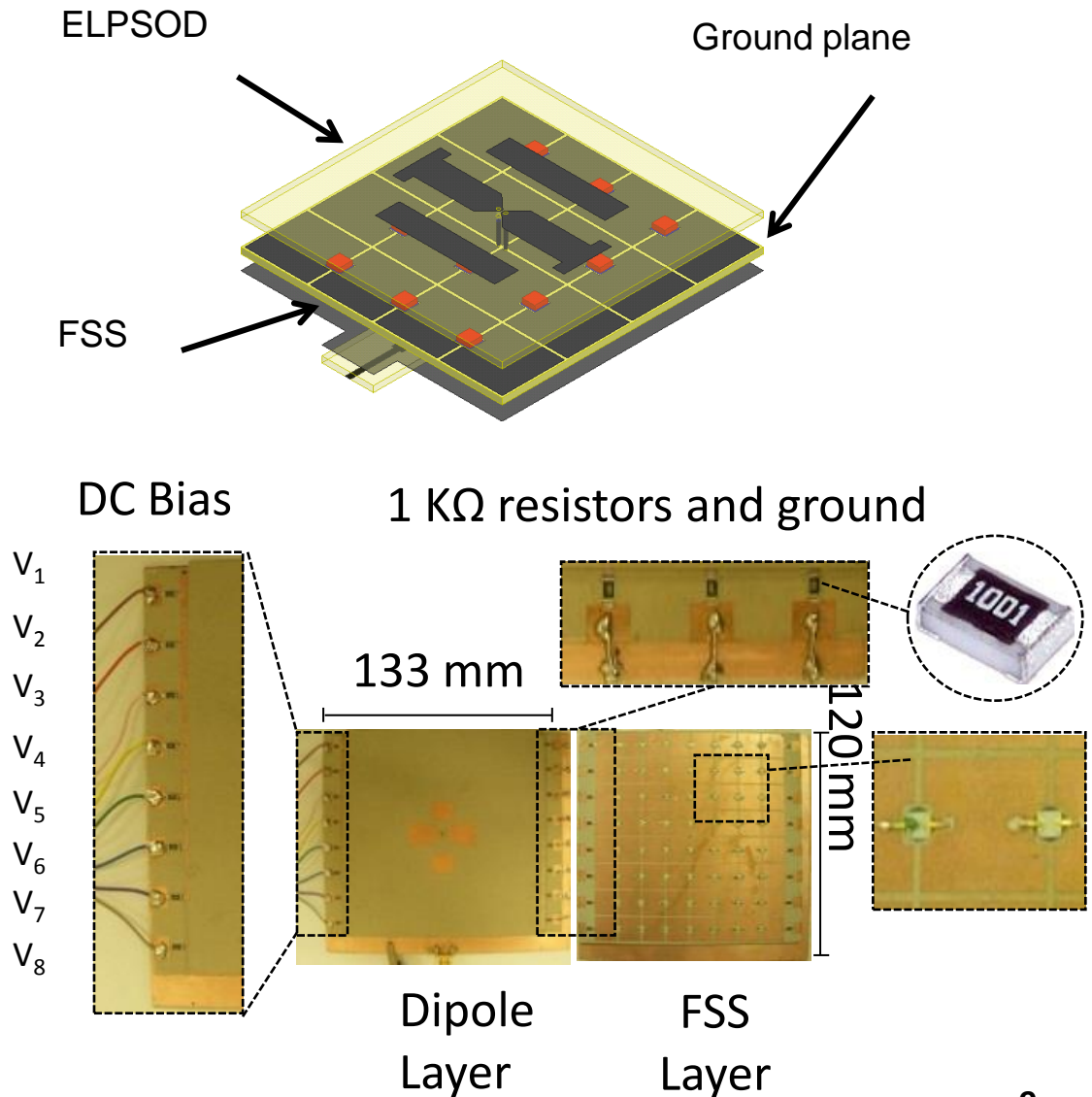
- End-Loaded Planar Open-Sleeve (ELPOSD)
- Broadband or dual response
- Tunable: Several parameters
- $L_p$  affects the upper resonance frequency
- $L$  affects the Lower resonance frequency



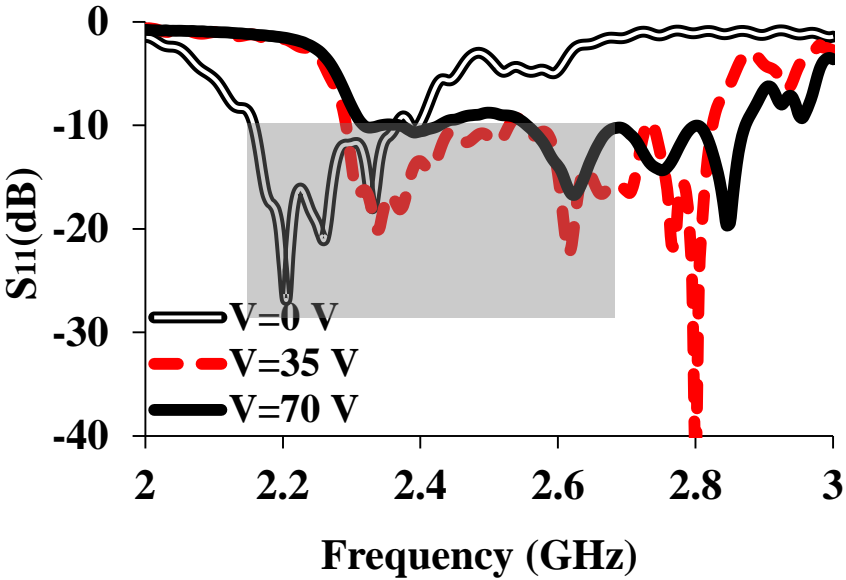


# 1-D Varactor based Tunable Antenna

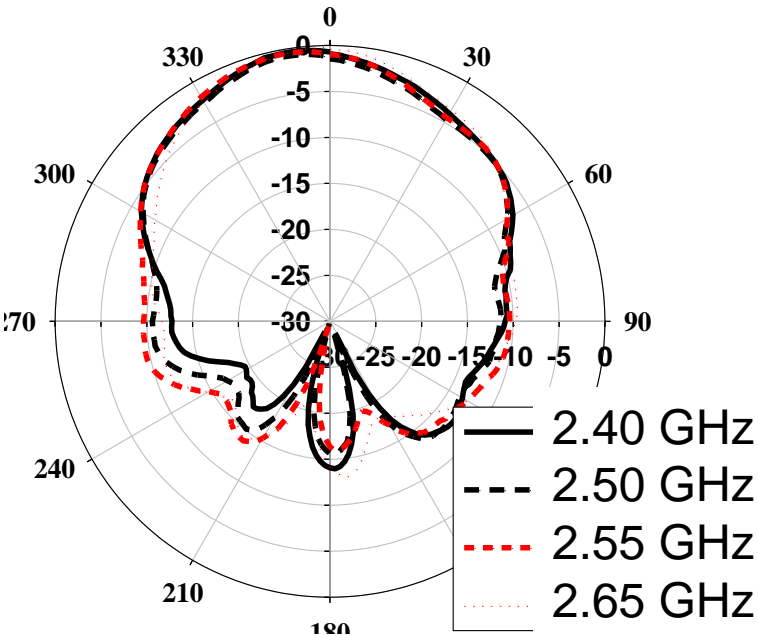
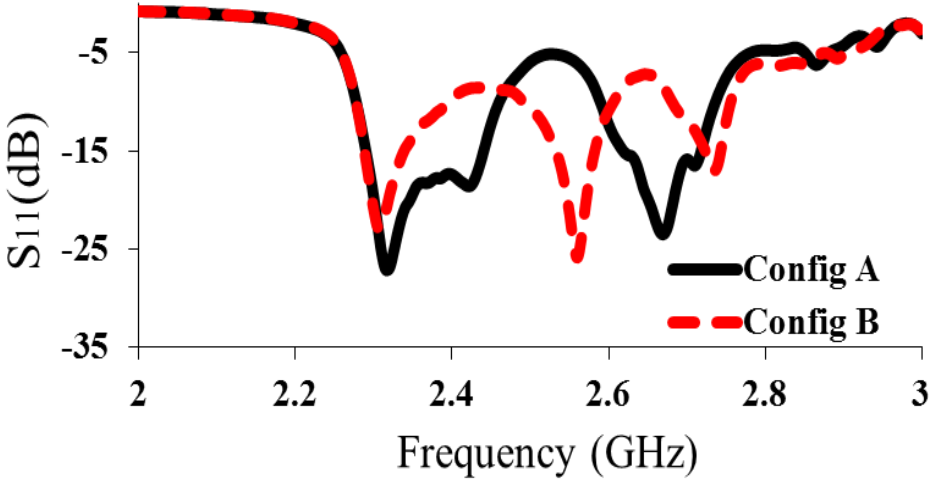
- Height  $\sim \lambda/45$  at 2.4 GHz
- Bias and fabrication simplicity
- Minimize the use of vias (potentially conformal nature)
- High front-to-back radiation pattern ratio
- Ability to dynamically adjust the center frequency



# Common bias applied



# Non-uniform bias voltages

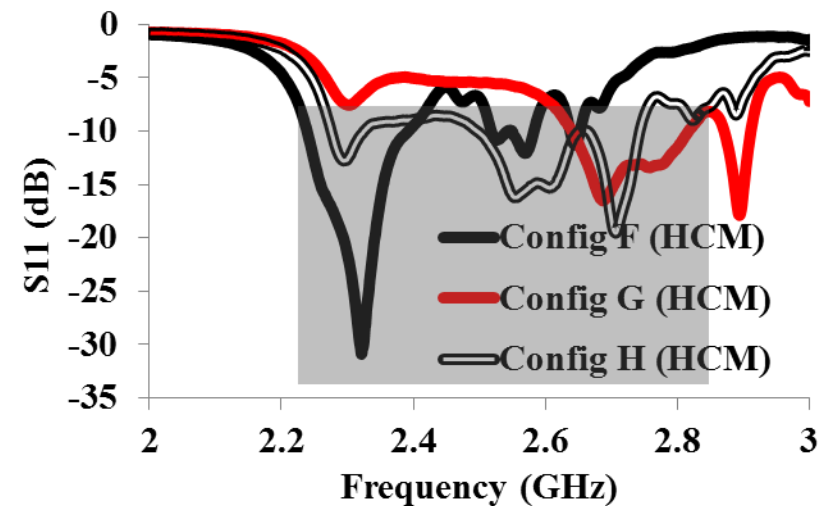
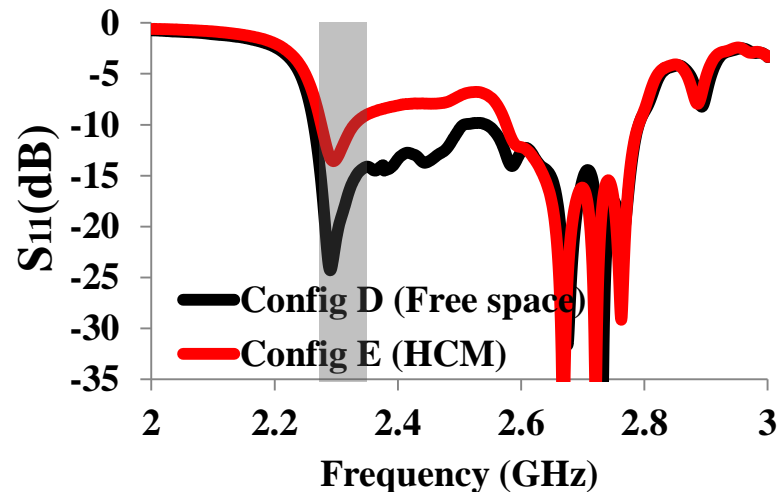


Config	$V_1, V_2$	$V_3$	$V_4, V_5$	$V_6$	$V_7, V_8$
A	30 V	30 V	30 V	30 V	30 V
B	70 V	70 V	30 V	70 V	70 V

# Operation using non-uniform bias voltages with Human Core Model (HCM)



Config.	$V_1, V_2$	$V_3$	$V_4, V_5$	$V_6$	$V_7, V_8$
D (No HCM)	30 V	30 V	30 V	30 V	30 V
E (w/ HCM)	30 V	30 V	30 V	30 V	30 V
F (w/ HCM)	10 V	30 V	30 V	30 V	20 V
G (w/ HCM)	50 V	30 V	30 V	30 V	50 V
H (w/ HCM)	100 V	100 V	100 V	100 V	100 V

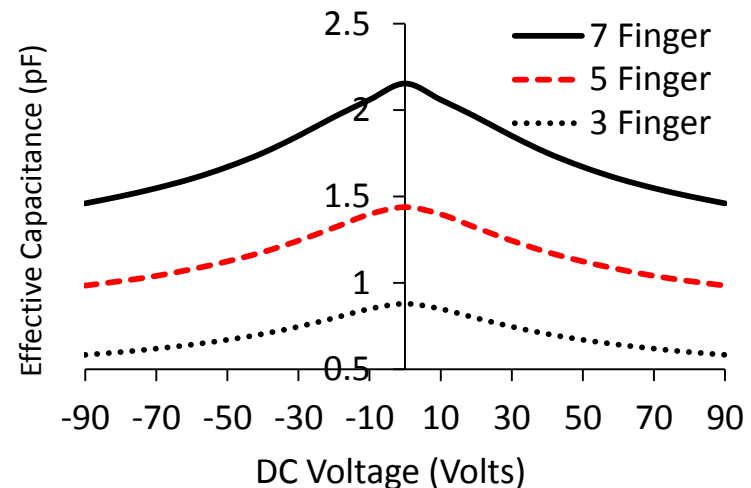
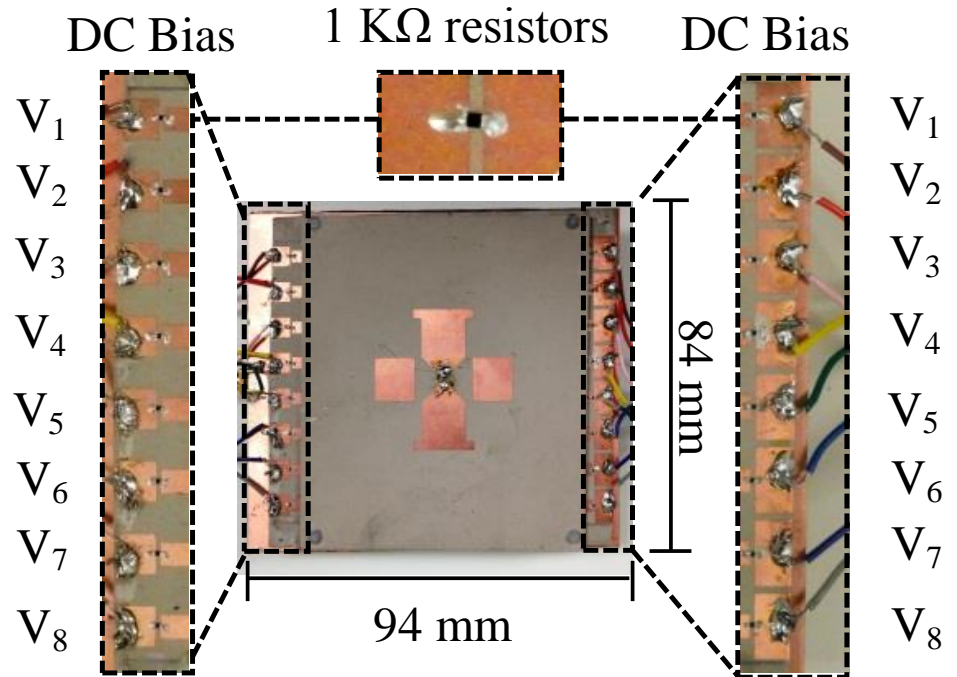


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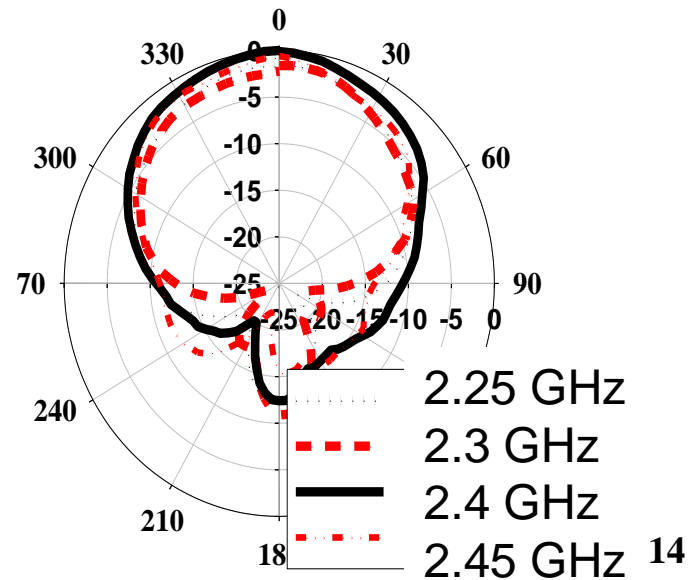
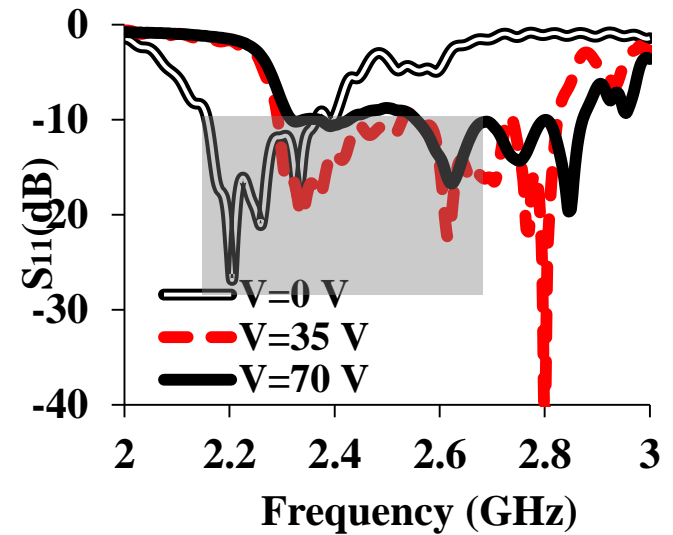
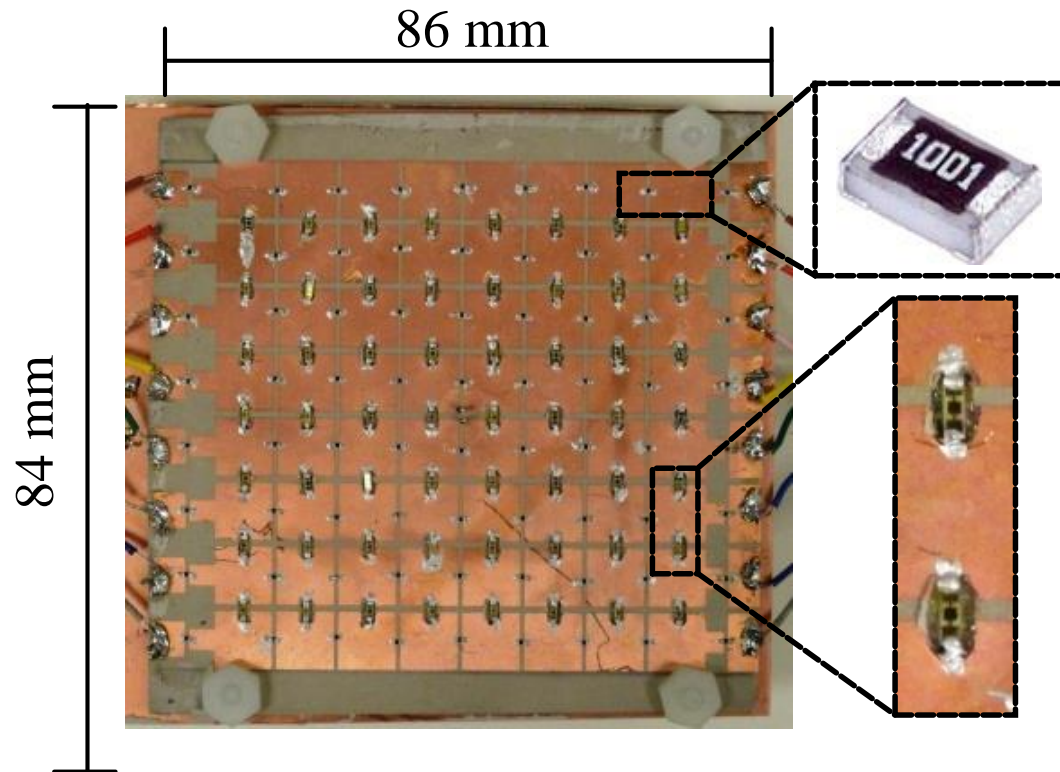
## **1-D BST VARACTOR BASED ANTENNA**

# BST Varactor Based antenna

- Height  $\sim \lambda/45$  at 2.4 GHz
- Bias and fabrication simplicity
- Take advantage of the C-V symmetry curve
- Avoid the use of vias (potentially conformal nature)
- High front-to-back radiation pattern ratio
- Ability to dynamically adjust the center frequency



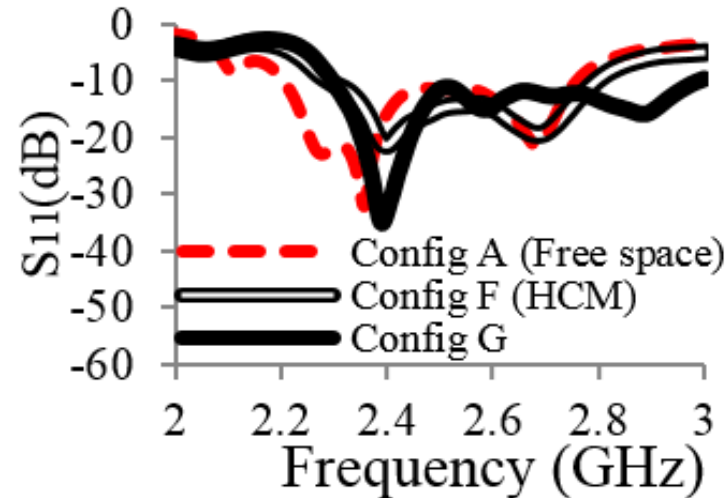
# FSS Layer Using Barium Strontium Titanate (BST) Varactors



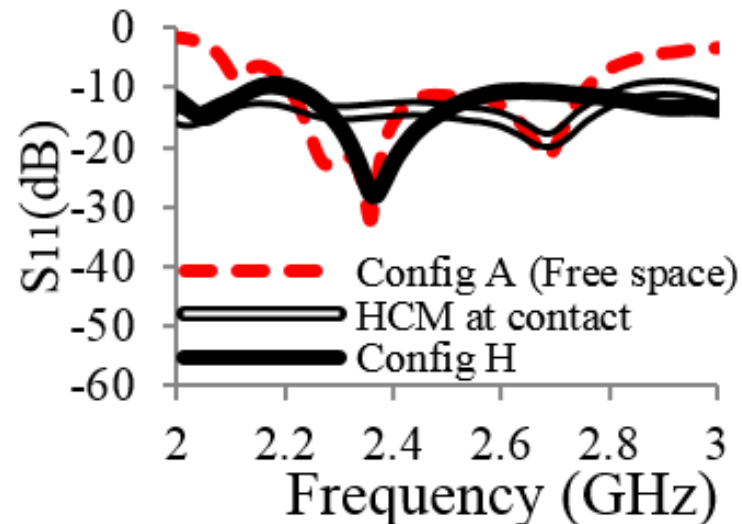
# Operation using non-uniform bias voltages with Human Core Model (HCM)

Impedance match adjustment in:

- Close proximity to a HMC



- At contact with HMC



# GaAs vs. BST antenna

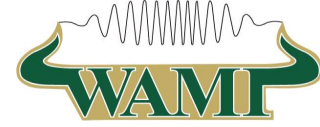
Antenna	Mass (gms)	Total devices	Cost per device	Cost	Area (mm <sup>2</sup> )	Eff. (%)	Tunable BW (MHz)
GaAs	188	56	50 US\$	High	15600	50-80	520
BST	87	56	0.1 US\$	Low	7900	30-60	425

## ■ GaAs vs BST varactor based antenna

- Both - low profile
- Both - Easily tunable
- BST - Reduced planar size and mass compared to GaAs
- BST- Cost effective
- BST - Compact and robust

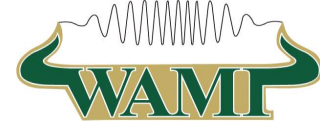


# Summary



- A low profile, tunable dipole antenna using BST varactors has been demonstrated
- The total antenna thickness is  $\sim \lambda/45$  when using 1-D varactor-loading
- A tunable frequency response from 2.2 to 2.55 GHz
- Cost effective, compact, robust, easily tunable and low profile antenna
- BST varactor antenna enables:
  - Small bias Network voltages
  - Potential use of flexible substrates

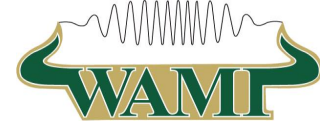
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# References

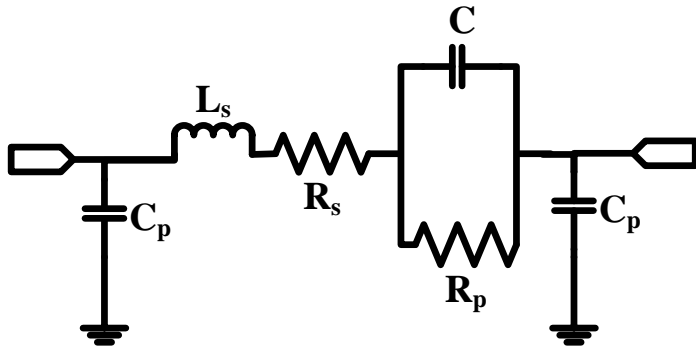


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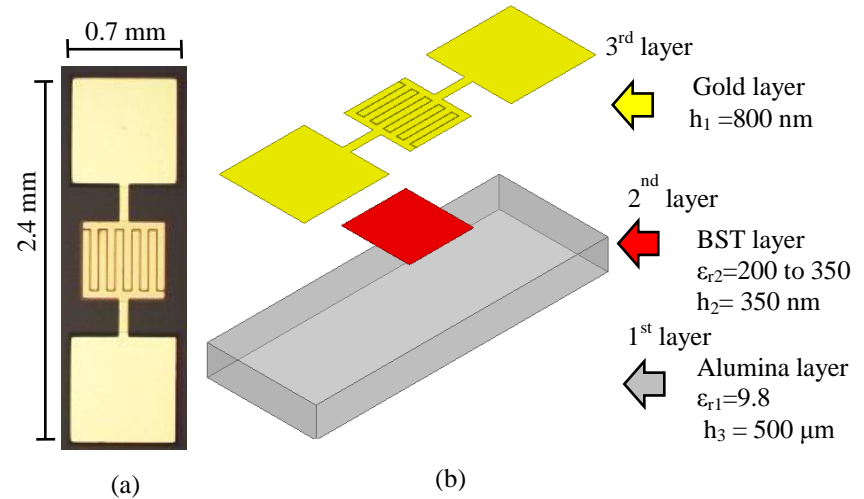
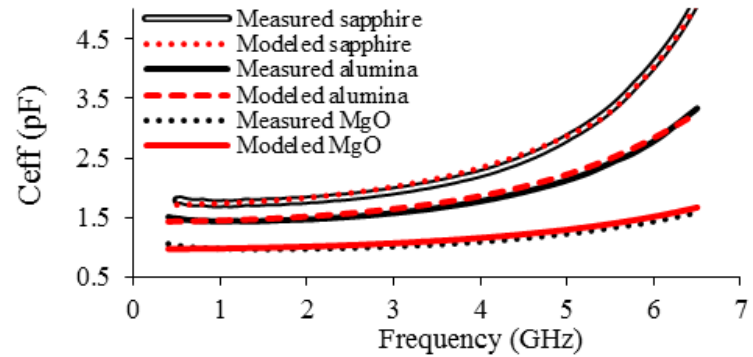
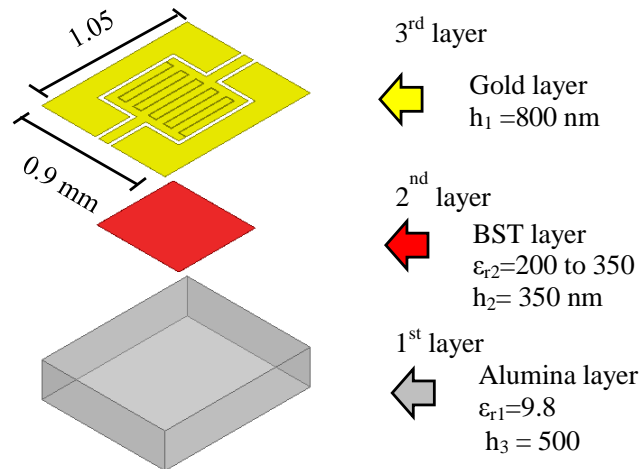
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- [11] M. Hosseini and M. Hakkak, “Characteristic estimation for Jerusalem Cross Based artificial magnetic conductors,” IEEE Antennas and Wireless Propag. Letter s, Vol. 7, 2008.
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# Add. 1 BST Varactor Characterization



Schematic for diode simulation.



## Add. 2

$$C_{end} = 4ns(2 + \pi)\epsilon_{end}\epsilon_0 \frac{K(\kappa_{0end})}{K(\kappa'_{0end})} \quad \begin{matrix} 54\% \\ \text{error} \end{matrix} \quad (4.9)$$

$$C_{end} = 2ns\left(2 + \frac{\pi}{2}\right)\epsilon_{end}\epsilon_0 \frac{K(\kappa_{0end})}{K(\kappa'_{0end})} \quad \begin{matrix} 6\% \\ \text{error} \end{matrix} \quad (4.10)$$

Number of Fingers	Measured Effective Capacitance at 0 volts	Measured Effective Capacitance at 90 volts	Permittivity extracted at 0V and 90 V (HFSS)	Permittivity extracted at 0V and 90 (Eq. 4.09)	Permittivity extracted at 0V and 90V (Eq. 4.10)
3	1.17 pF	0.88 pF	800-500	400-250	750-510
5	2.1 pF	1.5 pF	750-500	450-270	770-500
7	3.2 pF	2.2 pF	750-500	470-270	800-520

Number of Fingers	Measured Effective Capacitance at 0 volts	Measured Effective Capacitance at 90 volts	Permittivity extracted at 0V and 90 V (HFSS)	Permittivity extracted at 0V and 90 (Eq.4.09)	Permittivity extracted at 0V and 90V (Eq.410)
3	0.75 pF	.5 pF	350-230	160-70	350-200
5	1.4 pF	0.98 pF	350-230	180-90	360-210
7	2.1 pF	1.45 pF	350-230	200-100	370-220